TEE, an estimator for the precision of eclipse and transit minimum times

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ABSTRACT

Context. Transit or eclipse timing variations have proven to be a valuable tool in exoplanet research. However, no simple way to estimate the potential precision of such timing measures has been presented yet, nor are guidelines available regarding the relation between timing errors and sampling rate.

Aims. A timing error estimator (TEE) equation is presented that requires only basic transit parameters as input. With the TEE, estimating timing precision for actual data and for future instruments, such as the TESS and PLATO space missions, is straightforward.

Methods. A derivation of the timing error based on a trapezoidal transit shape is given. We also verify the TEE on realistically modelled transits using Monte Carlo simulations and determine its validity range, exploring in particular the interplay between ingress/egress times and sampling rates.

Results. The simulations show that the TEE gives timing errors very close to the correct value, as long as the temporal sampling is faster than transit ingress/egress durations and transits with very low S/N are avoided.

Conclusions. The TEE is a useful tool for estimating eclipse or transit timing errors in actual and future data sets. In combination with a previously published equation to estimate period-errors, predictions for the ephemeric precision of long-coverage observations are possible as well. The tests for the TEE’s validity range also led to implications for instrumental design. Temporal sampling has to be faster than transit ingress or egress durations, or a loss in timing precision will occur. An application to the TESS mission shows that transits close to its detection limit will have timing uncertainties that exceed 1 h within a few months of their acquisition. Prompt follow-up observations will be needed to avoid “losing” their ephemerides.

Key words. methods: data analysis – techniques: photometric – ephemerides – planets and satellites: detection – occultations – binaries: eclipsing

1. Motivation for an estimator of eclipse and transit timing errors

The precise timing of stellar eclipses and planetary transits has a long track record in astronomy, and numerous methods have been developed to measure the times of minimum brightness in eclipse-like events (e.g. Kwee & van Woerden 1956; Winkler 1967; Mikulášek et al. 2006; Oshagh et al. 2012). Eclipse minimum times, translated into variations of orbital periods, have been widely used in the analysis of eclipsing binary systems. More recently they also became important in the analysis of light curves from transiting exoplanets. In this case, deviations from strict periodicity, known as transit timing variations (TTVs), have usually been taken as indications of the presence of additional bodies in the system (e.g. Agol et al. 2005; Holman & Murray 2005; Heyl & Gladman 2007). In such cases, it is important to ensure that a supposed TTV\textsuperscript{1} is really due to an astrophysical effect and not an artefact of observational noise. This requires a technique to estimate the precision of the measured transit ephemerides. This need for an estimation of timing and ephemeris errors also arose during the ground-based photometric follow-up of planet candidates from the CoRoT space mission (Deeg et al. 2009). In this case, a reliable estimator of the timing error was necessary to determine when and if follow-up photometric observations of a transit candidates should be scheduled: if the expected timing error exceeded a few hours, the observations would not be conclusive. During the course of the mission, we became aware that the errors in the ephemerides given to us, which had been derived by other members of the CoRoT team, varied by factors of “a few” for candidates with similar basic parameters, like brightness, transit depth, and transit duration. Their ephemerides and their errors had been derived via a variety of methods, mostly by the fitting of different types of models – from trapezoid-shaped to more elaborate ones – but also eye estimates were used on occasion. A simple and reliable estimator for deriving timing errors was therefore desirable in order to perform follow-up observations with little delay, which led to the method presented here. In combination with the estimator for period-errors presented in Deeg (2015), predictions for the time-uncertainty of future transits, which are essential for any follow-up observations, could now be performed quickly.

This work is distinct from other, similar works in the literature. The original work on the subject, which in part inspired

\footnote{In the remainder of this work, we use the terms “transit” and “eclipse” interchangeably.}
this work, appeared in Doyle & Deeg (2004). In that work the authors describe the timing error for triangular-shaped binary eclipses. This was later extended by Sybilski et al. (2010), who explored the detectability of TTVs in binary star systems for the purpose of detecting circumbinary planets. They used a single eclipsing binary model and a single set of observing parameters (integration time, noise) for CoRoT and Kepler simulations and a few for ground-based simulations, ultimately verifying the equations presented in Doyle & Deeg (2004). Carter et al. (2008) present analytic approximations for transit light-curve observables, among them an equivalent equation for the timing uncertainty. Mighell & Plavchan (2013) and Deeg (2015) discuss ephemeris errors from continuous sets of timing measurements covering multiple orbital periods, as given by data from space missions like CoRoT and Kepler. These two papers, however, do not contemplate the expected timing precision of individual transit events, whose validation is the core of the present work.

Combining the work presented here and that by Deeg (2015) provides the tools for deriving both the epoch and the period-error of any linear ephemerides that are based on continuous-coverage data, needing only basic eclipse or transit parameters. We expect this work to be of particular interest for the study of the significance of transit timing variations (TTVs) and for the evaluation of the timing precision that can be expected in future instruments, such as the upcoming TESS and PLATO missions.

In the following, we present the formulae to derive timing errors of individual transits, which we refer to as the timing error estimator (TEE). By using a trapezoidal approximation for the transit shape, it is possible to derive an analytical expression for the timing error of an individual transit based on a few basic parameters. We concentrate on the derivation of the timing error of individual eclipses and extend this by assessing the impact of sampling rate on the timing error. We begin by exploring trapezoidal model eclipses to verify that the expression works as expected, then extend it to real modelled exoplanetary transits.

2. Eclipse timing error estimator, TEE

The derivation of TEE arises from the use of a trapezoid to approximate the shape of the eclipse where the flat part is of any length, including zero. Furthermore, it assumes that the parameters of the trapezoid (amplitude and durations of ingress, flat part and egress) are known with negligible errors, such that the only free parameter is the eclipse mid-time. Given these assumptions, let us consider the ingress of an eclipse (Fig. 1), with a depth of 1% or $\Delta F = 0.01$. The observations are simulated by taking a model trapezoid and adding white noise, at a level of $\sigma_{F_{\text{rms}}} = 0.002$ in the given case. In real observations, the level of white noise would be derived from out-of-eclipse data. The white noise level during the ingress is then $\sigma_{F_{\text{rms}}}$, $\sigma_{F_{\text{rms}}}/\sqrt{N_{\text{in}}}$, where $N_{\text{in}}$ is the number of points during ingress. In the event that the noise does not scale in this fashion, e.g. due to strong red noise, then $\sigma_{F_{\text{rms}}}$ should be determined by other means. The levels of $\pm \sigma_{F_{\text{rms}}}$ relative to the trapezoid are shown as dashed lines in Fig. 1. These lines also correspond to the expected 1σ errors when fitting the known model ingress to the data when the only free parameter is the time of ingress. The slope $T_{\text{rms}}/\Delta F$ then determines the corresponding error in time, given as $\sigma_{T_{\text{rms}}} = \sigma_{F_{\text{rms}}}/T_{\text{rms}}/\Delta F$.

Considering that observations will generally contain both ingress and egress, the only change is that instead of using only $\sigma_{F_{\text{rms}}}$, we should use the photometric noise on the timescale of ingress and egress summed, $\sigma_{F_{\text{rms}}}$, with $T_{\text{rms}}$ being the summed duration of ingress and egress (the $\nabla$ symbol denotes ingress plus egress, and is motivated by their triangular shape). This leads to the most basic form of the TEE:

$$\sigma_{T_{\text{rms}}} = \frac{\sigma_{F_{\text{rms}}}}{\Delta F},$$

where $\sigma_{T_{\text{rms}}}$ denotes the timing precision and $T_{\text{rms}} \approx 2T_{\text{in}}$ was used.

We also define a timing signal-to-noise, $(S/N)_h$, given by

$$(S/N)_h = 2\Delta F/\sigma_{F_{\text{rms}}}. \tag{2}$$

The relative timing error, $\sigma_{T_{\text{rms}}}/T_{\text{rms}}$, is then simply the inverse of $(S/N)_h$:

$$\frac{\sigma_{T_{\text{rms}}}}{T_{\text{rms}}} = \frac{1}{(S/N)_h}. \tag{3}$$

Normally, the noise of the data on the timescale $T_{\text{rms}}$ is not well known, but will be known on another timescale $\tau$ (e.g. over the sampling time between data points). We propose, therefore, a white noise scaling from the known noise $\sigma_{F_{\text{rms}}}$ over the timescale $\tau$ to the noise $\sigma_{F_{\text{rms}}}$ using

$$\sigma_{F_{\text{rms}}} = \sigma_{F_{\text{rms}}} \frac{\sqrt{\tau}/T_{\text{rms}}}{\sqrt{T_{\text{rms}}}/\tau}, \tag{4}$$

where we assume that the number of data points is proportional to the length of the timescales $\tau$ and $T_{\text{rms}}$. This leads then to this general form of the TEE:

$$\sigma_{T_{\text{rms}}} = \frac{\sigma_{F_{\text{rms}}}}{2\Delta F} \sqrt{\tau/T_{\text{rms}}}. \tag{5}$$

For convenience, we also provide this equation in terms of the ingress time $T_{\text{in}} = T_{\text{rms}}/2$:

$$\sigma_{T_{\text{rms}}} = \frac{\sigma_{F_{\text{rms}}}}{2\Delta F} \sqrt{\frac{T_{\text{in}}}{2}}. \tag{6}$$

In real time-series data, conversions between noises on the different timescales often deviate strongly from white noise scalings.\footnote{While Eq. (1) uses relative values for the photometric noise $\sigma_{F_{\text{rms}}}$ and the transit amplitude $\Delta F$, we note that for small amplitudes $\Delta F$, the use of magnitude units for both parameters will lead to identical results.}

Fig. 1. Model of an eclipse ingress of $\Delta F = 0.01$ (solid line) with simulated data (crosses). The dotted lines outline the $\sigma_{F_{\text{rms}}}$ = 0.002 standard deviation of the individual data points, and the dashed lines outline the expected error of the average over all 50 points within the ingress.
when timescales differing by more than an order of magnitude are considered. It is therefore advisable to characterise the noise on a timescale that is not very different from \( T_\gamma \) when using TEE. For example, when we predicted the timing precision of CoRoT transits, we used the photometric noises over a timescale of \( \tau = 2 \, \text{h} \) given by Aigrain et al. (2009). This timescale is suitable as it is of the same order of magnitude as the \( T_\gamma \) of the transit candidates. On the other hand, a scaling from the point-to-point errors of CoRoT data would lead to an underestimation of the timing precision, due to a significant red noise component on a two-hour timescale relative to CoRoT’s standard sampling time of 512 s (Aigrain et al. 2009). However, if a white noise scaling from the point-to-point noise, \( \sigma_{F, \text{in}} \), to \( \sigma_{F, \text{c}} \) is acceptable, we may also use a version of the TEE in terms of the number of points during ingress-plus-egress, \( n_\tau \), with \( n_\tau = T_\gamma / \tau \) (here \( \tau \) is the time between exposures):

\[
\sigma_t = \frac{\sigma_{F, \text{in}} \, T_\gamma}{2 \, \Delta F / \sqrt{n_\tau}} \tag{7}
\]

We note that the above equation is well-suited for Kepler data since no relevant red noise (Jenkins et al. 2010) affects the scaling from the nominal 30-min sampling time of Kepler long-cadence data to the hour-long ingress/egress durations of most planet transits, represented by \( T_\gamma \).

3.3. Behaviour of the TEE for naturally occurring transits

The use of a trapezoidal shape in the first sets of simulations was motivated by the use of that same shape for the derivation of the TEE in order to determine the TEE’s fundamental correctness and range of validity. The predicted relative timing error \( \sigma_t / T_\gamma \) depends only on one parameter, \( (S/N)_t \) (see Eq. (2)), but the range of \( (S/N)_t \) for which the TEE is reliable was uncertain. Also uncertain was the range of validity of the TEE against another parameter that can be expected to affect the timing precision, the number of data points during ingress and egress, \( n_\tau \).

We used a Monte Carlo approach to obtain the \( \sigma_{t, \text{meas}} \). For each of the 10 000 Monte Carlo trials, we generated time series with a specified sampling rate and level of white noise, and then inserted a trapezoidal event with a given value of \( n_\tau \) and \( (S/N)_t \) at a random time \( t_c \) safely away from either end of the time series. Then, assuming a priori knowledge of the shape of the trapezoid, we determine its mid-time \( t_c \) from a simple \( \chi^2 \) minimisation. We obtained a \( \Delta t_c \) from each trial by taking the difference between the input and output \( t_c \), keeping the \( \chi^2 \) as an indication of the quality of the fit. The measured timing precision \( \sigma_{t, \text{meas}} \) was then obtained from the standard deviation of the \( \Delta t_c \) from the 10 000 trials. This process was then repeated for each set of input parameters \( n_\tau \) and \( (S/N)_t \).

The results from these simulations are shown in Fig. 2, expressed as the ratio between the measured timing precision and that predicted by the TEE, \( \sigma_{t, \text{meas}} / \sigma_t \). This ratio approaches 1, meaning that the TEE performs a valid prediction of the timing precision, if two conditions are met: \( n_\tau > 2 \) and \( (S/N)_t \gg 10 \). On the other hand, if the sampling rate or the \( S/N \) is below these limits, the real timing precision may be much worse than that given by the TEE.

Equation (3) shows that for \( S/N_t \leq 1 \), no useful timing error can be measured as \( \sigma_t \) will exceed the length of an ingress or egress. In practice – and shown by the simulations – more stringent limits of \( S/N_t \) apply since with decreasing \( S/N \), the reliability of eclipse detections decreases and contributions from random detections with arbitrary \( \Delta t_c \) values become relevant.

3.2. Behaviour of the TEE for naturally occurring transits

Now that the TEE against trapezoid-shaped transits has been validated, we extend here the analysis to natural eclipse shapes as these are of more practical interest. These tests are more complex than for the trapezoidal models that we used previously, as values such as \( T_\gamma \) and \( \Delta F \) are no longer input variables for the tests and must instead be approximated in some way in order to evaluate the accuracy of TEE. In theory, it should be possible to perform a numerical analysis of a model transit in order to calculate these values exactly. However, for the purposes of this study (which only attempts to evaluate the errors in timing, but not errors in other transit parameters) it is sufficient to fit trapezoids to naturally shaped transits, as this will deliver the parameters that are relevant for the TEE. To that end, we proceeded with the following steps:

i) A set of noiseless model light curves was generated from pixelated representations of a stellar disc that is occulted...
by a transiting planet, employing the same method as the UTM transit modeller (Deeg 2014). All light curves were generated for transits of a planet of 0.09 stellar radii across a solar-like star, while the following parameters were varied step-wise, leading to a total of 480 combinations: The impact parameter of the transit was incremented in eight steps, from an equatorial transit with \( b = 0 \) to a nearly polar (but still total) transit with \( b = 0.9 \). Models were generated with six different sampling rates, where the coarsest models represented the entire transit in six points and the finest ones represented it in 360 points. All models were generated for two visual passbands, namely \( V \) and \( I \), using the corresponding quadratic solar limb-darkening coefficients. All of these models were then normalised such that the deepest part of the fitting process. In either case, the lowest \( S/N \) corresponds to one of the possible parameter combinations.

ii) For each of these noiseless transit models, we obtained a trapezoidal fit and converted its output into the parameters relevant for the TEE, namely \( \Delta F \) and \( \tau \) respectively \( \sigma_m \). Since the models were those of real transits, the \( \Delta F \) of the best-fit trapezoids was always lower than the 1% flux decrease of the input models. Also, owing to the nature of the trapezoidal fit, the resulting fit duration was always longer than the transit duration of the input models.

iii) For each set of input parameters we performed 10 000 injection and retrieval trials. For each trial light curve, random white noise at one of the levels specified in step i) was added to the noiseless models and the transit mid-time was offset by a random amount, which was recorded.

iv) On each of the trial light curves, we used the noiseless natural transit shape (obtained in step i) to perform a one-parameter fit for the transit mid-time, and recorded the difference between the fitted mid-time and the input mid-time.

v) The subsequent analysis proceeded similarly to that in Sect. 3.1. From the distribution of input-output differences from each of the 10 000 trials, we obtained the measured timing precision \( \sigma_{t,\text{meas}} \) and compared it to the TEE estimate \( \sigma_t \), which was based on the parameters from step ii) and the known noise \( \sigma_m \). This was done for each parameter set, with the ratio \( \sigma_{t,\text{meas}}/\sigma_t \) determining the colour of the points in Fig. 3.

We note that the use of a noiseless model in step ii) to obtain the transit parameters except mid-time corresponds to the usual procedure employed in the analysis of long-coverage light curves. There, transit parameters are derived from phase-wrapped superpositions of multiple individual transits, resulting in a light curve with a higher \( S/N \) than that of the individual transits from which the timing measurements are obtained.

The bulk of the sets in Fig. 3 show a ratio \( \sigma_{t,\text{meas}}/\sigma_t \) close to one, demonstrating that a trapezoidal fit to the transit is sufficient to estimate the expected timing error. However, a close comparison with the results from the trapezoidal tests depicted in Fig. 2 shows some subtle differences: reduced detectability for low values of \( (S/N)_h \), improved performance around \( (S/N)_h \approx 7 \), and in general a better performance for low values of \( n_T \). This is due to the fact that real transits have some curvature all the way through the transit. The \( T \) derived from the trapezoidal fit therefore underestimates the true effective value of this parameter, which mitigates the detrimental effects of low sampling rates. The differences for low \( (S/N)_h \) may be real or may be an artefact of the fitting process. In either case, the lowest \( S/N \) cases have timing errors \( \sigma_t \) that approach or exceed the transit duration and neither are the transits themselves reliably detected.

4. An example application: Timing precision of TESS detections

In the following, we show an application of the TEE towards the estimation of the timing precision of transiting planets (or planet candidates) detected by the TESS mission. TESS (Ricker et al. 2014, 2015) is a NASA mission slated for launch in late 2017 that will survey nearly the entire sky for transiting planets, with the majority of the sky being covered by single pointings lasting 27.4 days. This relatively short observational coverage may lead to concerns regarding the precision of the ephemerides of the transiting objects found, since ephemerides with large uncertainties may make the re-observation of a planet (or candidate, it does not matter in this context) very difficult. This becomes the case once a predicted transit has timing errors larger than 2–3 h, which makes the appearance of that transit in a given observing night rather uncertain. During the photometric follow-up of CoRoT planet candidates (Deeg et al. 2009), this concern also surfaced, especially for candidates with shallow transits or for those found in “short-run” pointings of less than 50 days. It led to the implementation of a timing-precision estimator for all candidates (Deeg et al. 2012) and motivated follow-up observations of all detected planets, aimed at refining their ephemerides to a precision that maintains timing errors below 1 h over at least one decade (Deeg et al. 2015). Table 1 shows five groups of examples with the timing precision that can be expected from TESS.
| $R_p$ | $R_*$ | $P_{tr}$ | $N_{tr}$ | $I_C$ | $\alpha$ | $\Delta F$ | $(S/N)_{06}$ | $T_\gamma$ | $N_c$ | $\sigma_\gamma$ | $(S/N)$ | $\alpha_{\delta P}$ | $\alpha_{\Delta t}$ | sample (ii–v: relative to i) |
|------|------|--------|--------|------|--------|-----------|-------------|---------|--------|--------|-----------|-----------|-------------|----------------|--------------------|
| 2    | 1    | 9      | 3      | 8.7  | 115    | 0.034     | 10.0        | 509     | 4.2    | 305    | 2.2       | 231       | 210         | 1.68          |
| 2    | 0.3  | 9      | 3      | 12.8 | 1020   | 0.37      | 8.7         | 778     | 6.5    | 2193   | 3.4       | 229       | 208         | 1.66          |
| 4    | 1    | 9      | 3      | 11.3 | 407    | 0.13      | 11.4        | 1018    | 8.5    | 766    | 3.5       | 290       | 264         | 2.11          |
| 4    | 0.3  | 9      | 3      | 14.5 | 3685   | 1.49      | 9.9         | 1556    | 13.0   | 5604   | 5.3       | 292       | 266         | 2.13          |
| 2    | 1    | 9      | 3      | 8.2  | 67     | 0.03      | 17.2        | 509     | 4.2    | 178    | 3.8       | 135       | 123         | 0.98          |
| 2    | 0.3  | 9      | 3      | 10.3 | 233    | 0.37      | 38.1        | 778     | 6.5    | 500    | 14.9      | 52        | 47          | 0.38          |
| 4    | 1    | 9      | 3      | 8.8  | 123    | 0.13      | 37.8        | 1018    | 8.5    | 231    | 11.6      | 88        | 80          | 0.64          |
| 4    | 0.3  | 9      | 3      | 12.0 | 601    | 0.19      | 60.5        | 1556    | 13.0   | 914    | 32.6      | 48        | 43          | 0.35          |
| 5    | 1    | 9      | 3      | 8.7  | 115    | 0.21      | 63.6        | 1272    | 10.6   | 193    | 21.7      | 59        | 53          | 0.43          |
| 5    | 0.3  | 9      | 3      | 12.8 | 1020   | 0.13      | 16.5        | 706     | 4.2    | 231    | 11.6      | 88        | 80          | 0.64          |
| 2    | 0.3  | 9      | 3      | 10.3 | 233    | 0.37      | 14.2        | 706     | 4.2    | 231    | 11.6      | 88        | 80          | 0.64          |
| 5    | 0.3  | 9      | 3      | 12.0 | 601    | 0.19      | 60.5        | 1556    | 13.0   | 914    | 32.6      | 48        | 43          | 0.35          |
| 5    | 1    | 9      | 3      | 8.7  | 115    | 0.21      | 63.6        | 1272    | 10.6   | 193    | 21.7      | 59        | 53          | 0.43          |
| 5    | 0.3  | 9      | 3      | 12.8 | 1020   | 0.13      | 16.5        | 706     | 4.2    | 231    | 11.6      | 88        | 80          | 0.64          |
| 2    | 0.3  | 9      | 3      | 10.3 | 233    | 0.37      | 14.2        | 706     | 4.2    | 231    | 11.6      | 88        | 80          | 0.64          |

Table 1. Transit timing precision and ephemeris precision of example transit detections by the TESS mission; see text for details.

It also shows the corresponding precision of the ephemeris that may be obtained. The columns of that table are, from left to right, as follows:

- $R_{pl}$, $R_*$: sizes of the planet and the star.
- $P_{tr}$, $N_{tr}$: period of the planet and the number of transits that are observed by TESS, assuming its predominant temporal coverage of 27.4 days.
- $I_C$: target magnitude in the $I_C$ band of TESS. This band is at the centre of the TESS passband.
- $\sigma_\gamma$: expected 1σ photometric precision for a target with given $I_C$ magnitude over 1 h integration time. This value was taken from the “total precision” for a given magnitude in Fig. 8 of Ricker et al. (2015).
- $\Delta F$: relative depth of a transit, assuming $\Delta F = (R_{pl}/R_*)^2$, e.g. without limb-darkening.
- $(S/N)_{06}$: signal-to-noise of the planet detection in the entire sequence of transits. This value is derived for a circular orbit of the planet around its central star, with the transit durations derived from Kepler’s third law, assuming equatorial transits and a stellar mass given by the empirical mass-radius relation for main-sequence stars (Demircan & Kahraman 1991): $M_\star \approx \text{const} \times (L_\star /L_{\odot})^{1/4}$.
- $T_\gamma$: the duration of the combined ingress and egress time for an equatorial transit.
- $N_C$: number of data points in $T_\gamma$, the sum of ingress and egress time. The TESS time-sampling of 2 min is used.
- $\sigma_{T,1yr}$: precision of the planet’s ephemeris 1 yr after the first transit was detected by TESS. For this value, Eq. (18) of Deeg (2015) was used, assuming $\sigma_\gamma$ to be the ephemeris epoch (or zero-point) error. The dominant term of $\sigma_{T,1yr}$ is, however, the period-error $\sigma_p$.

The first four cases (sample i) correspond to planet detections at the limiting $I_C$ magnitude indicated by a revised version\(^5\) of Fig. 3 of Sullivan et al. (2015), who define a detection as “achieving a signal-to-noise ratio greater than 7.3 from 6 h of integration time during transits”. Since our assumptions led to somewhat longer total on-transit integration times, the $(S/N)_{06}$ of the four examples given augments to values around 10. These four examples were selected to cover the range of stellar sizes that constitute the principal sample of TESS, and to cover the range of planet-sizes for which Sullivan et al. calculated limiting magnitudes.

The next three samples ii)–iv) are identical to sample i) except for the modification of a single parameter. In sample ii), the target stars are 10 times (or 2.5 mag) brighter; in sample iii) the radii of the planets have been multiplied by 2.5 (the larger planets are now about Jupiter-sized), and in sample iv) the orbital period has been divided by 3, leading to three times as many transit events. In sample v), both the planet size and the target brightness have been increased relative to the cases at the detection limit.

Regarding the interpretation of these calculations, first we note that in all cases, the derived timing precision are lower than the limits to the timing precision. This is due to the assumption

\[ \sigma_{T,1yr} = \text{const} \times (12/(N_C^2 - N_{tr}^2))^{1/2}. \]

\(^5\) During the preparation of this work, we noted a significant discrepancy between a detection S/N that was scaled from Sullivan et al.’s value of 7.3 and a detection S/N that was derived from first principles. After contacting Sullivan et al., they found an error in their Fig. 3 and provided a revised version with limiting magnitudes that are 1.5–3 mag brighter (Errata to Sullivan et al. 2015, in prep.). They indicated that the error that affected their Fig. 3 does not have consequences on any other results of their paper.

A93, page 5 of 7
of equatorial transits, where ingress/egress times are shortest, and is due to neglecting stellar limb-darkening, which also leads to ingress/egress times that may be shorter (but never longer) than real transit ingresses/egresses, in which the inner part often displays a notable rounding as well. Even with these shortest-possible ingress/egress times, we find that $N_e$ is $\geq 3$ in all cases, meaning that the TESS two-minute sampling interval is sufficiently short to avoid any degradation of the timing precision.

For the cases at the faint detection limit (sample i), their theoretical timing error $\sigma_t$ is 4–5 min, while the error of the ephemerides of such planets (or planet candidates) will be about 2 h after one year. A further warning on the observability of these detections arises from their low timing signal-to-noise ($S/N)_t$ As our simulations in Sect. 3 show, true timing errors will exceed the theoretical errors for $(S/N)_t \leq 10$. Transits with timing errors of 2 h can usually still be recovered in single-night follow-up observations; but given above warning, a rapid follow-up within a few months is advisable, before multi-night or multi-site campaigns may become required in order to “recover” the transits of these detections at the limit of TESS.

For samples ii) and iii), with a detection $S/N$ of 20–60, we expect that one year after the observations by TESS, their ephemeris errors will be on the order of one hour. That is, a follow-up within about one year after their detection is advisable. Sample iv) evaluates the gain from shorter orbital periods. The timing precision of individual transits ($\sigma_t$ in Table 1) improves only slightly over sample i), due to the shorter ingress and egress times ($T_{\text{egress}}$). The larger number of observed transits, however, leads to an improvement in the ephemeris precision ($\sigma_{P_t}/P$ and $\sigma_{T_t}/T_t$) by a factor of \(\approx 2\). For such planets, with a detection $S/N$ of 10–15, follow-up observations should also be performed within one year.

Only for sample v), with a detection $S/N > 200$, will TESS derive ephemerides that are sufficiently precise to permit re-observation of their transits for several years. A refinement of these ephemerides by a dedicated follow-up program would however be desirable as well, in order to obtain ephemerides that are sufficiently precise for useful transit predictions over timescales of 10 years or more.

5. Conclusions

In this work we have introduced and validated the TEE, a formula that permits a quick estimation of the expected timing precision of individual transits or eclipses. This is expected to be useful for estimates of timing precision for both ground- and space-based data. Together with the work by Deeg (2015) on period and ephemeris errors from time series covering multiple orbital periods, and assuming that there are no intrinsic period variations (e.g. transit timing variations, TTVs), we now have the tools at hand to estimate the precision of ephemerides for the majority of planet detections (those without TTVs) from rather basic assumptions, as is shown in the preceding example on TESS detections.

From the simulations shown in Sect. 3, we can conclude that the TEE accurately represents the timing precision of idealised trapezoidal eclipses, provided that the timing signal-to-noise is $(S/N)_t > 10$ and the number data points during ingress and egress, $n_e$, is larger than 2. While Eq. (3) shows that no useful timing error can be measured for $(S/N)_t \leq 1$, as $\sigma_t$ will exceed the length of an ingress or egress, in practice such low values of $(S/N)_t$ are not expected to occur as they would have originated from detections below usual detection thresholds. The TEE also predicts the timing error of naturally occurring transits, for which it is sufficient to obtain the TEE’s required parameters from trapezoidal fits to the transits. Moreover, the limitations on timing precision from low $n_e$ seem to have a lesser effect on natural transits as they have, in general, no truly flat portions – it is not the flat portion of a trapezoidal eclipse that contributes to the timing precision, but the slopes of the ingress/egress. We note that one of the assumptions in the TEE are negligible errors in its input parameters (e.g. the depth of the transit). Considering that the TEE does not estimate a value but an error – for which 1–2 digit precision is sufficient – this assumption should not have consequences in practical applications. In any case, relevant uncertainties of the input parameters will occur only in the low $S/N$ regime, where our simulations have already shown that the results from the TEE lead to underestimations of the real timing error. We emphasise here that the TEE is not intended to generate “final” publication-quality timing errors if a full transit modelling is feasible.

The results from our simulations also have implications for the observational design of instruments acquiring photometric time series. As a general rule, eclipses or transits should be observed with cadences that are shorter than the expected ingress or egress duration (e.g. $n_{\text{avg}} > 1$ is desirable). Beyond this, and assuming that a white noise scaling is valid, the number of data points during ingress or egress has little effect on the real timing precision or on the reliability of prediction made with the TEE.

As an example of this, the Kepler/K2 mission obtained most of its time series with its “long-cadence” (29.4 min) sampling. For eclipsing bodies that are small or have short periods, ingress/egress times shorter than 30 min are frequently encountered. The timing precision of these short-period objects would have been substantially better if they had been observed with cycle times a half or a quarter as long as the long cadence. For example, Ford et al. (2011) indicate an improvement in the timing error of the KOI-137 system (published in parallel as Kepler 18 by Cochran et al. 2011) of a factor of 2 for its short-cadence (=1 min sampling) data relative to its long-cadence data.

Regarding the TESS mission, our calculations on expected ephemeris precision have shown that for transiting planets found near the TESS detection limit, a photometric follow-up to acquire further transit times should be performed within one year after their initial detection, in order to maintain their future observability. Also, for the majority of its expected planet discoveries, further photometric follow-up will be required in order to establish ephemerides that guarantee their long-term observability.

This will not be a worry with the PLATO space mission, foreseen to be launched by ESO in late 2025. This mission will observe large swaths of the sky with campaigns lasting 2–3 years (Rauer et al. 2014) while its nominal sampling rate of 25 s (with bright objects being sampled at a rate of 2.5 s) greatly exceeds the requirements for precision timing of any kind of normal planet-star system. This rapid sampling may have other benefits as well, such as a more reliable recovery of the shapes of eclipses from short-period orbiters or the precise timing of eclipses across compact objects, such as white dwarfs, where total eclipse durations of the order of minutes may be encountered.

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