

# Dynamics of solar coronal loops

## I. Condensation in cool loops and its effect on transition region lines

D. A. N. Müller<sup>1</sup>, V. H. Hansteen<sup>2</sup>, and H. Peter<sup>1</sup>

<sup>1</sup> Kiepenheuer-Institut für Sonnenphysik, Schöneckstr. 6, 79104 Freiburg, Germany  
e-mail: peter@kis.uni-freiburg.de

<sup>2</sup> Institute of Theoretical Astrophysics, University of Oslo, PO Box 1029, Blindern 0315, Oslo, Norway  
e-mail: Viggo.Hansteen@astro.uio.no

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**Abstract.** We report numerical calculations of the condensation of plasma in short coronal loops, which have several interesting physical consequences. Firstly, we propose a connection between small, cool loops ( $T < 10^6$  K), which constitute one of the basic components of the solar transition region, and prominences, in the sense that the same physical mechanism governs their dynamics: Namely the onset of instability and runaway cooling due to strong radiative losses. Secondly, we show that the temporal evolution of these loop models exhibits a cyclic pattern of chromospheric evaporation, condensation, motion of the condensation region to either side of the loop, and finally loop reheating with a period of 4000–8000 s for a loop of 10 Mm length. Thirdly, we have synthesized transition region lines from these calculations which show strong periodic intensity variations, making condensation in loops a candidate to account for observed transient brightenings of solar transition region lines. Remarkably, all these dynamic processes take place for a heating function which is *constant* in time and has a simple exponential height dependence.

**Key words.** Sun: corona – Sun: transition region – Sun: UV radiation

### 1. Introduction

Since Skylab, loops have been recognized as a vital ingredient in coronal structure and coronal energetics. Indeed, one could imagine that the corona is entirely composed of nested loops with varying lengths, temperatures, heating rates, and activity levels. A nested structure of low-lying cool loops was suggested by Dowdy et al. (1986) to explain the temperature dependence of the emission measure. Thus, building an understanding of loop energetics is obviously a desirable objective. There are alternative scenarios for the structure of the transition region (see, e.g., Mariska 1992). As recent SOHO/SUMER results have shown, however, small cool loops to constitute one of the basic building blocks of the transition region (Feldman et al. 2000), this paper will concentrate on the dynamics and energetics of cool loops.

The main components in the energy balance of *static* loops were identified by Rosner et al. (1978): They consist of the unknown heating, thermal conduction and radiative losses in the loop itself and at the transition region/chromosphere boundary. Roughly speaking one can understand static loop behavior quite well by assuming that the heat deposited by the heating

mechanism in the corona is largely conducted back towards the chromosphere where it is radiated away. Due to the strong temperature dependence of the thermal conduction coefficient, this scenario almost invariably leads to apex loop temperatures of roughly 1 MK bounded by a geometrically small transition region as the temperatures fall towards  $10^4$  K and chromospheric densities at the loop footpoints. Variations in the heating rate are dealt with in this type of loop by chromospheric evaporation or coronal condensation such that the radiative losses at the top of the chromosphere balance the thermal conductive flux from above (Hansteen 1993). This behavior is almost independent of the details of the heat deposition – as long as radiative losses near the loop apex are not an important factor in the energy budget.

Clear as the model above seems, serious difficulties are encountered as soon as loop model predictions are confronted with the observations themselves. These difficulties are various and sundry (Mariska 1992) but might be summarized as follows: The differential emission measures predicted by the models gives a much lower line emission from the lower transition region, below  $10^5$  K, than what is observed (alternatively one could say that the line emission from the upper transition region, above  $10^5$  K, is predicted much too high). In addition it is very difficult to account for the pervasive *average* red shift

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Send offprint requests to: D. A. N. Müller,  
e-mail: dmueLLer@kis.uni-freiburg.de

of up to  $10 \text{ km s}^{-1}$  seen in lower transition region lines and blue-shifts in the upper transition region and low corona (Peter & Judge 1999).

Several proposals have been put forward to answer the difficulties outlined above. Dowdy et al. (1986) suggested a two-component transition region, consisting of magnetic funnels and a nested structure of low-lying, cool coronal loops. This new class of static loop solutions had been discussed by Antiochos & Noci (1986). Cally & Robb (1991) argued, however, that these cool loop solutions were unstable, and Cally (1990) proposed turbulent thermal conduction as an alternative hypothesis to explain the enhanced transition region emission. As for the spectral diagnostics of transition region lines, loop dynamics due to downward-propagating magnetoacoustic waves were shown to be a candidate to account for the pervasive redshifts (Hansteen 1993).

However, it was first with the observations by the SOHO and TRACE instruments that the importance of cool loops and loop dynamics has belatedly come to the foreground. Peter (2000) gives evidence for a multi-component structure of the transition region, and Feldman et al. (2001) reach the conclusion that regions of hotter and cooler plasma in the solar atmosphere are essentially disconnected from each other.

The question that is raised is what implications these new ideas have on our understanding of the structure and energetics of both cool and hot coronal loops. Obviously a time-dependent heating will produce a number of dynamic phenomena such as waves or material motions through evaporation or condensations. But as we will show below it is also found that within a certain parameter range of static mechanical energy deposition quite violent dynamics can ensue.

Numerous mechanisms of coronal heating have been proposed (e.g. wave heating, nanoflares, magnetic reconnection), but independent of the detailed process of energy release there is now observational evidence that coronal loops are predominantly heated at the footpoints (Aschwanden et al. 2000, 2001). With heating concentrated near the loop footpoints it is no longer certain that sufficient energy to counter radiative losses is deposited near the loop apex. In fact, for such loops static solutions with a hot midpoint may no longer exist as the radiative loss rate increases strongly in the loop center when the temperature decreases towards  $T \approx 2 \times 10^5 \text{ K}$ . If the magnetic field topology is such that the loop has a dip in the center, footpoint heating can lead to the condensation of plasma in the loop center and hence give rise to prominence formation (Antiochos et al. 1999). It was also found by Antiochos et al. (2000) that this type of prominence formation shows a cycle of formation, motion, and destruction. Recently, it was demonstrated by Karpen et al. (2001) that the condition of a “dipped” geometry is indeed not a necessary condition for prominence formation in long loops (their work describes a loop of 340 Mm length). A key element in their prominence scenario is the large ratio of loop length to the damping length of the heating function, and the authors argue that shorter loops with a smaller ratio should therefore behave differently.

We present numerical calculations which show that, depending on the damping length of the heating function, condensation is also possible in short, cool coronal loops. We study

the evolution of these loops, discuss static as well as dynamic solutions and finally calculate the time-dependent emission of transition region lines arising from this model.

## 2. Numerical model

We numerically solve the time-dependent hydrodynamic equations for conservation of mass, momentum and energy in one spatial dimension, coupled with the ionization rate equations for several elements and self-consistent radiative losses (cf. Hansteen 1993, for details). The modeled plasma is subjected to gravitational acceleration equal to that found on the solar surface. Thermal conduction, radiative losses and a coronal heating term are included in the energy equation.

The equations for mass conservation, momentum, energy, and ionization and recombination rates read as follows:

- Mass conservation:

$$\rho \frac{\partial v}{\partial t} + \frac{\partial}{\partial z}(\rho v) = 0. \quad (1)$$

- Momentum equation:

$$\rho \frac{\partial v}{\partial t} + \rho v \frac{\partial v}{\partial z} = \frac{\partial}{\partial z}(p + \Lambda) - \rho g_{\parallel}. \quad (2)$$

- Energy equation:

$$\frac{\partial}{\partial t}(\rho e) + \frac{\partial}{\partial z}(\rho v e) + (p + \Lambda) \frac{\partial v}{\partial z} = -\frac{\partial F_c}{\partial z} + Q_m - L_{\text{rad}} + Q_o. \quad (3)$$

- Rate equations:

$$\frac{\partial n_{ij}}{\partial t} + \frac{\partial}{\partial z}(n_{ij}v) = n_e \left[ n_{i-1} C_{i-1} - n_{ij} (C_{ij} + \alpha_{ij}) + n_{i+1} \alpha_{i+1} \right]. \quad (4)$$

Here  $v$  denotes the velocity along the curvilinear loop coordinate,  $z$ ,  $g_{\parallel}$  the component of the gravitational acceleration that is parallel to the magnetic field,  $Q_m$  the mechanical heating rate,  $L_{\text{rad}}$  the radiative loss rate per unit volume, and  $Q_o$  a small “opacity heating” term that is included in order to maintain chromospheric temperatures at roughly 7000 K. The internal energy,  $e$ , is calculated as the sum of the thermal and internal energy including only ionization states, the contribution from the excitation energy is negligible. The population of the ionization state  $j$  of element  $i$  is denoted by  $n_{ij}$ , while ionization rates and recombination rates are represented by  $C_{ij}$  and  $\alpha_{ij}$ , respectively. The artificial viscosity term  $\partial \Lambda / \partial z$  (according to von Neumann & Richtmyer 1950) is discussed by Hansteen (1993). The thermal conduction is set to  $F_c = \kappa_0 T^{5/2} dT/dz$  (Spitzer 1962) with  $\kappa_0 = 1.1 \times 10^{-11} \text{ W m}^{-1} \text{ s}^{-1} \text{ K}^{-7/2}$ .

Radiative losses are computed assuming that the plasma is effectively thin. While, ideally, one should solve the equation of radiative transport in order to calculate the radiative losses, comparisons with models where this has been done (Carlsson 2003; Kuin & Poland 1991) indicate that the errors incurred by assuming effectively thin losses in the  $\text{Ly}_\alpha$  line are not significant to the energetics of the system in the upper chromosphere and above. Radiative losses are due to collisional excitation

of the various ions comprising the plasma. We have included the elements hydrogen, helium, carbon, oxygen, neon, and iron in the radiative losses, as well as thermal bremsstrahlung, using the ionization and recombination rates given by Arnaud & Rothenflug (1985) and Shull & van Steenberg (1982) and the collisional excitation rates found through the HAO-DIAPER atomic data package (Judge & Meisner 1994). The collisional excitation rate from the ground state of hydrogen to its first excited state is computed from coefficients found in Janev et al. (1987). Some of the metals are treated by assuming ionization equilibrium and then deriving an a priori radiative loss curve as a function of electron temperature. On the other hand radiative losses from the ions specifically mentioned in this study, i.e. losses from hydrogen, helium, carbon and oxygen, are computed consistently with full time-dependent rate equations.

The equations are formulated on a staggered, adaptive grid using the Reynolds transport theorem as described by Winkler et al. (1984) and the adaptive grid formulation suggested by Dorfi & Drury (1987). Particle and momentum fluxes are calculated according to the second-order upwind method of Van Leer (1974). This results in a set of equations which are solved implicitly by means of the Newton-Raphson scheme to advance the equations in time.

### 2.1. Loop heating

In order to parametrize the energy input into the coronal loop, we specify the energy flux amplitude at the footpoints of the loop,  $F_{m0}$ , and assume a mechanical heat flux that is constant up to a height  $z_1$  and then decreases for  $z \geq z_1$  as

$$F_m(z) = F_{m0} \exp[-(z - z_1)/H_m] \quad (5)$$

with a damping length  $H_m$ .

We will vary  $H_m$  between 0.25 and 3.25 Mm in the models presented below. For the mechanical energy flux we adopt the value of  $F_{m0} = 150 \text{ W m}^{-2}$  (the same as the one used by Hansteen & Leer 1995), and set  $z_1 = 1.75 \text{ Mm}$  for a loop of 10 Mm length.

The heating rate, i.e. the energy deposition per unit time and unit volume, is given by the divergence of the energy flux:

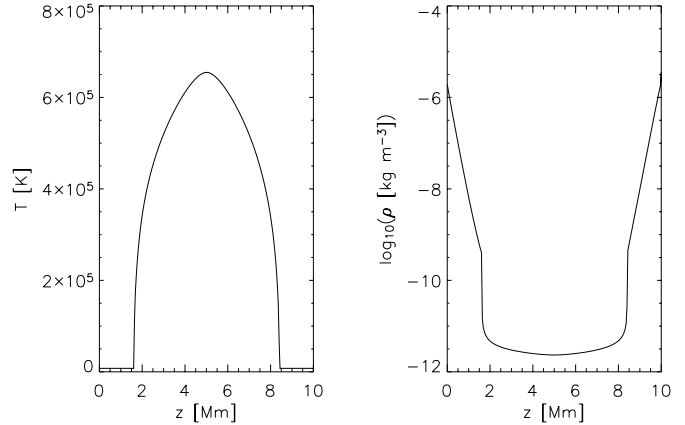
$$Q_m(z) = -\frac{A_0}{A} \frac{dF_m(z)}{dz} = \frac{A_0}{A} \frac{F_m(z)}{H_m}. \quad (6)$$

We consider a loop of low  $\beta$  plasma and assume a constant cross section of the loop, i.e.  $A = A_0 = \text{const}$ . This parametrization of the heating function was first suggested by Serio et al. (1981) and seems to be supported by recent observations (Aschwanden et al. 2000, 2001). Special care was taken to normalize the heating rate to a given energy flux in order to separate effects from changes of the amplitude of the energy flux to changes in its spatial distribution.

## 3. Results: Condensation due to thermal instability

### 3.1. Initial state

Our model coronal loop has a total length of 10 Mm, consisting of a semicircular arch of 8 Mm length and a vertical stretch



**Fig. 1.** Initial configuration: temperature,  $T$  (left), and particle density,  $\rho$  (right), along the loop with a total length of 10 Mm.

of 1 Mm length at both ends. In Fig. 1 we show the initial loop configuration. The temperature and density are plotted as a function of distance,  $z$ , along the loop. At the base we find a total particle density of  $n_{\text{base}} = 8.8 \times 10^{20} \text{ m}^{-3}$ . This density corresponds (very) roughly to a height of  $h = 605 \text{ km}$  above  $\tau_{500 \text{ nm}} = 1$  in the Vernazza et al. (1981) quiet sun model. The ionization degree of hydrogen is  $\approx 0.3\%$  at this height in our model. The base temperature is set to  $T_{\text{base}} = 7000 \text{ K}$ .

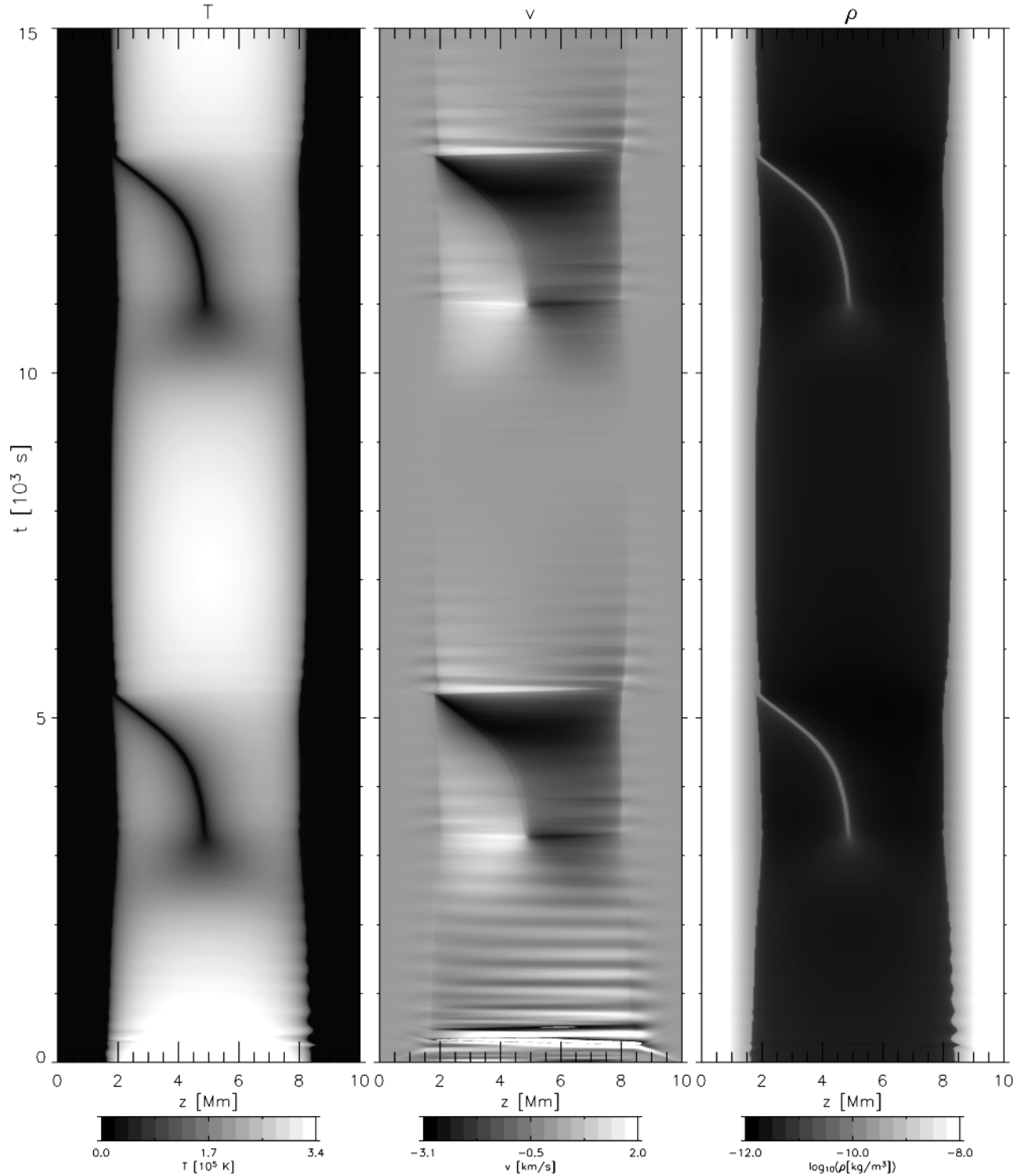
In the chromosphere, the temperature remains constant while the density falls off exponentially with a scale height of about 190 km until the transition region is encountered at 1.6 Mm. Here the temperature rises rapidly reaching  $10^5 \text{ K}$  at 1.63 Mm and  $5 \times 10^5 \text{ K}$  at 2.81 Mm. The loop apex temperature is  $6.55 \times 10^5 \text{ K}$ .

Energy losses by radiation are  $L_{\text{rad}} \approx 10^{-4} \text{ W m}^{-3}$  in the coronal and transition region portions of the loop while conductive losses to the top of the chromosphere account for  $\nabla Q \approx 8 \times 10^{-4} \text{ W m}^{-3}$ , i.e. the loop is essentially a “hot loop” in that the energetics are dominated by conduction.

The sound crossing time for the loop is 7 min and a low amplitude acoustic wave is initially bouncing in the coronal portion of the loop between the two steep temperature gradients. This wave had been triggered by a temporally and spatially localized energy deposition (*nanoflare*) in the upper part of the loop. This episodic heating mechanism was switched off before the start of the simulation, and replaced by the continuous heating function given by Eq. (6). All calculations presented here could have equally well been initialized with a static loop model, but we decided to start with this perturbed model in order to illustrate that the formation of recurrent condensations is not only possible when starting from an analytic solution, but also for dynamic, and therefore more “realistic” circumstances.

### 3.2. Loop evolution

Starting from the loop described above, we prescribe a *time-independent* heating function as given by Eq. (6) with a damping length of  $H_m = 1.25 \text{ Mm}$ , which results in a heating rate at the loop center that is 15% of the maximal heating rate,



**Fig. 2.** Temporal evolution of temperature (*left*), velocity (*center*), and density (*right*) along the loop. The heating rate for the loop shown is characterized by  $F_{m0} = 150 \text{ W m}^{-2}$  and a scale height of  $H_m = 1.25 \text{ Mm}$ .

$Q_m(z_1)$ . At  $z = z_1 = 1.75 \text{ Mm}$ , the ratio of mechanical heating to radiative losses is 0.26 at  $t = 0$ , while at the loop apex, it is 2.10.

The evolution of the loop temperature, velocity, and density is shown in Fig. 2. During the first 2300 s the loop cools down from  $T_{\text{top}}(t = 0) = 6.5 \times 10^5 \text{ K}$  to  $T_{\text{top}}(t = 900 \text{ s}) = 2 \times 10^5 \text{ K}$ ,

while the density stratification remains roughly constant and the low amplitude acoustic wave continues to bounce between the two transition regions.

At  $t = 2300 \text{ s}$  there is a sudden change: The temperature at the loop apex is no longer the maximal loop temperature, and this dip in the temperature stratification amplifies rapidly.

At the same time, a flow towards the cooling loop apex sets in, which reaches  $v \approx 2 \text{ km s}^{-1}$  at  $t = 3200 \text{ s}$ . At  $t = 3400 \text{ s}$ , a clump of cool ( $10^4 \text{ K}$ ) material with rapidly increasing mass content has formed at the loop apex. This clump, which we call the *condensation region* hereafter, eventually starts moving slowly towards one loop leg and is accelerated to  $v \approx 3 \text{ km s}^{-1}$  before draining into the chromosphere at  $t = 5300 \text{ s}$ . As a result, a weak rebound shock forms on the left side, followed by a phase of chromospheric evaporation which refills the evacuated loop with plasma. This upflow decreases with time from  $v(t = 5400 \text{ s}) \approx 1.5 \text{ km s}^{-1}$  to  $v(t = 8000 \text{ s}) \approx 0$ . In the meantime, the apex temperature of the loop has reached its maximum of  $T_{\text{max,top}} = 3.4 \times 10^5 \text{ K}$  at  $t = 7200 \text{ s}$ . The subsequent decline in temperature is first slow and then becomes faster towards  $t = 10\,000 \text{ s}$ . At this time a dip in the temperature profile forms again at the loop apex, and the whole process repeats.

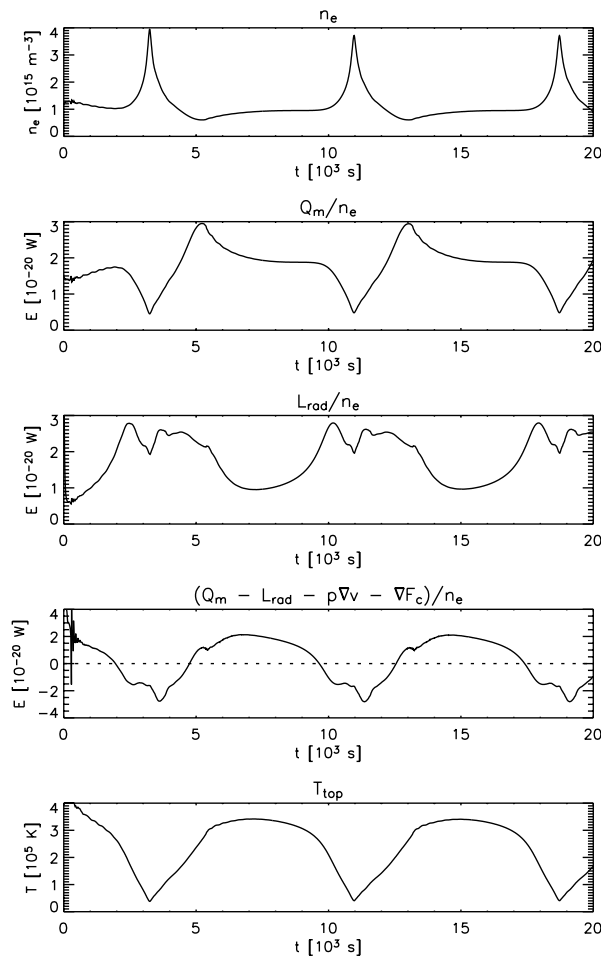
In the case of the model run shown in Fig. 2, a slow magneto-acoustic wave of low amplitude passes through the loop in the beginning of the simulation and leads to a leftward motion of the condensation region. Alternatively, an asymmetry of 1% between the deposited energy in both legs proved to be sufficient to dictate the draining direction: the condensation region then moves to the side on which less energy is supplied.

### 3.3. Energy balance analysis

The formation of the central dip of the temperature stratification results from the concentration of heating near the footpoints of the loop or, to put it differently, from insufficient heating at the top. In order to better understand the evolution of the loop, let us consider the energy balance at the loop apex for a damping length of  $H_m = 1.25 \text{ Mm}$ . The relevant terms for this are the mechanical energy supply,  $Q_m$ , the radiative losses,  $L_{\text{rad}}$ , the adiabatic compression,  $p\nabla v$ , and the divergence of the conductive flux,  $\nabla F_c$ .

As the density in the coronal part of the loop increases, the mechanical heating *per particle*,  $Q_m/n_e$ , decreases (the ion density,  $n_{\text{ion}}$ , equals approximately the electron density,  $n_e$ ). This is displayed in the top row of Fig. 3. At the same time, the radiative losses per particle,  $L_{\text{rad}}/n_e$  (Fig. 3, center), increase as the temperature drops to  $T = 2 \times 10^5 \text{ K}$ , which is predominantly due to the temperature dependence of the radiative losses.

The time-dependence of the total energy balance at the apex is dominated by two interacting processes, namely the increase of radiative losses and the increase of density. The bottom plot of Fig. 3 shows that, as a result of this interplay, the energy supply at the loop top becomes negative at  $t = 2000 \text{ s}$ , which explains the developing dip in the temperature profile. The simultaneous decrease of the gas pressure initiates a symmetric flow towards the center of the loop, so that more and more mass is advected and a condensation region forms. Once the temperature dip has formed as a consequence of the described loss of equilibrium, a thermal instability sets in as  $L_{\text{rad}} \propto n_e^2$ . This process of runaway-cooling has been described, e.g., by Antiochos & Klimchuk (1991). As our model loop is of semi-circular shape, the configuration with a condensation region located at the very center of the loop is gravitationally unstable.



**Fig. 3.** Energy balance at the loop apex for a damping length of  $H_m = 1.25 \text{ Mm}$ . From *top to bottom*: electron density,  $n_e$ , mechanical heating per particle, radiative losses per particle, the sum  $(Q_m - L_{\text{rad}} - p\nabla v - \nabla F_c)/n_e$  per particle (negative values mean that the loop apex is losing energy), and the temperature at the loop top.

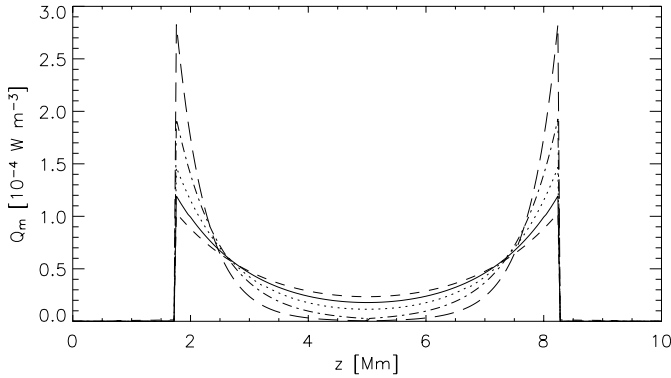
Therefore, the slightest perturbation forces the condensation region to move downward in either direction, where it experiences increasing acceleration as described below.

### 3.4. The role of the damping length

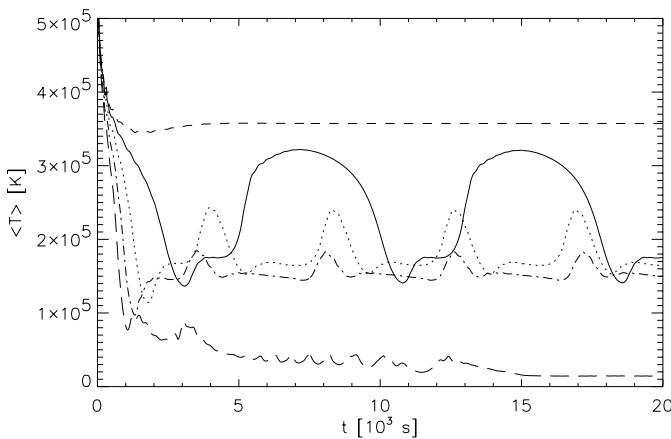
A plausible hypothesis is that the major factor in determining the cyclic behavior of the loop lies in the damping length,  $H_m$ , of the heating function because this critically influences the heat deposition at the loop top. We have studied the influence of the damping length on the thermal evolution of the loop by varying  $H_m$  from  $0.25 \text{ Mm}$  to  $3.25 \text{ Mm}$  and in each case letting the loop model evolve for  $20\,000 \text{ s}$ .

In Fig. 4, the mechanical heating function,  $Q_m(z)$ , is plotted for different values of  $H_m$ . The temporal evolution of the mean loop temperatures,  $\langle T \rangle$ , is displayed for these models in Fig. 5. For this plot, we define the mean temperature as the average temperature over the central half of the loop, i.e. from  $z = 2.5 \text{ Mm}$  to  $z = 7.5 \text{ Mm}$ .

Let us consider the limiting cases first: for short damping lengths of  $H_m \lesssim 0.5 \text{ Mm}$ , the loop decays as not enough energy



**Fig. 4.** The mechanical heating function,  $Q_m(z)$ , plotted for different values of  $H_m$ . Dashed line:  $H_m = 1.5$  Mm, solid line:  $H_m = 1.25$  Mm, dotted line:  $H_m = 1.0$  Mm, dash-dotted line:  $H_m = 0.75$  Mm, long-dashed line:  $H_m = 0.5$  Mm.



**Fig. 5.** The influence of the damping length,  $H_m$ , on the thermal evolution of the loop. Dashed line:  $H_m = 1.5$  Mm, solid line:  $H_m = 1.25$  Mm, dotted line:  $H_m = 1.0$  Mm, dash-dotted line:  $H_m = 0.75$  Mm, long-dashed line:  $H_m = 0.5$  Mm.

is deposited in the upper part of the loop to balance the radiative and conductive losses. In this case the temperature in the loop falls during the first 15000 s to roughly  $10^4$  K and stays at that level for the remainder of the model run, maintained in part by the “opacity” heating term.

On the other hand, for longer damping lengths with  $H_m \geq 1.5$  Mm, the energy deposition at the loop center is large enough to sustain a stable loop against radiative and conductive losses and an average loop temperature of  $3.6 \times 10^5$  K (for  $H_m = 1.5$  Mm) is reached and maintained (see Fig. 5, dashed). Even longer damping lengths lead to stable loops with slightly higher temperatures.

The regime in between, with intermediate damping lengths of  $0.75 \text{ Mm} \leq H_m < 1.5 \text{ Mm}$ , shows the cyclic behavior described above. In these cases, the loop exhibits a dynamic behavior, triggered by the onset of thermal instability as described in Sect. 3.2.

Extending the description of the model run analyzed in Sect. 3.2, we focus on the solid line in Fig. 5, for a damping length of  $H_m = 1.25$  Mm. The first minimum of this curve with  $\langle T \rangle_{\min} = 1.4 \times 10^5$  K is attained at  $t = 3000$  s, corresponding to the formation of the condensation region. This is

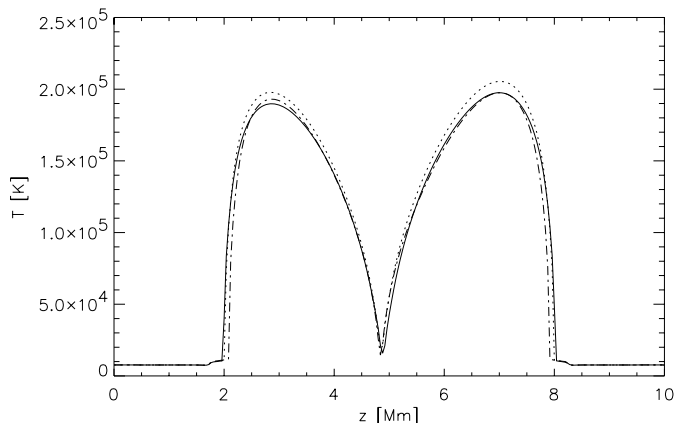
**Table 1.** Loop parameters for different damping lengths,  $H_m$ : Minimum mean temperature,  $\langle T \rangle_{\min}$ , maximum mean temperature,  $\langle T \rangle_{\max}$ , and corresponding linestyles in Figs. 4–6.

$H_m$ [Mm]	$\langle T \rangle_{\min}$ [ $10^5$ K]	$\langle T \rangle_{\max}$ [ $10^5$ K]	$P$ [s]	linestyle
0.5	0.1	0.1	$\infty$	— —
0.75	1.4	1.8	4600	- - - -
1.0	1.5	2.4	4100	.....
1.25	1.4	3.2	7800	— — — —
1.5	3.6	3.6	$\infty$	- - - -

followed by an increase in temperature towards a temporary plateau at  $\langle T \rangle = 1.8 \times 10^5$  K. During this phase, the condensation region is moving down one loop leg, while the top of the loop is already reheating. After the condensation region has left the loop, the temperature rises rapidly to  $\langle T \rangle_{\max} = 3.7 \times 10^5$  K at  $t = 7200$  s. At this point in time, the net energy supply at the loop top decreases (cf. Sect. 3.3), and the loop starts to cool gradually. When the temperature approaches  $T = 2 \times 10^5$  K, the radiative losses increase strongly which drastically accelerates the cooling process. As a result, a new condensation region forms, and a second minimum in mean temperature is attained at  $t = 10800$  s. The period of this condensation cycle is  $P = 7800$  s.

For the cases of shorter damping lengths,  $H_m = 0.75$  Mm and  $H_m = 1.0$  Mm, the formation of a condensation region works qualitatively in the same way. Let us therefore focus on the differences: As the heating is more strongly concentrated towards the footpoints of the loop, the net energy supply per particle at the loop top starts to decrease at an earlier point in time so that the maximum loop temperature attained is lower, namely  $T_{\max} = 2.2 \times 10^5$  K for  $H_m = 0.75$  Mm, and  $T_{\max} = 2.6 \times 10^5$  K for  $H_m = 1.0$  Mm compared to  $T_{\max} = 3.4 \times 10^5$  K for  $H_m = 1.25$  Mm. Due to the strong radiative losses towards  $T = 2 \times 10^5$  K, these loops subsequently also cool faster than the hotter loop, so that the period of the condensation cycle is shorter than for  $H_m = 1.25$  Mm:  $P = 4600$  s for  $H_m = 0.75$  Mm and  $P = 4100$  s for  $H_m = 1.0$  Mm. The cooling rate,  $\Delta T/\Delta t$ , in the temperature range  $1.5 \times 10^5 \text{ K} < T < 2.5 \times 10^5 \text{ K}$  is very similar for all three cases, which leads us to the conclusion that the increased period for the damping length of  $H_m = 1.25$  Mm is mostly due to the longer duration of loop reheating and loop cooling at temperatures  $T > 2.5 \times 10^5$  K. First tests with longer and hotter loops suggest that the cooling phase from  $T = T_{\max}$  up to the development of a dip in the temperature profile can indeed be much longer than any other phase of the condensation cycle. Table 1 summarizes the relevant parameters for different damping lengths.

It should be noted that for all loops which form a condensation region, the minimum mean temperature is very similar,  $\langle T \rangle_{\min} = 1.4\text{--}1.5 \times 10^5$  K. This minimum temperature is attained when the condensation region has just formed, which happens shortly after the dip in the temperature profile has developed. At this point in time, the energy balance, as discussed in Sect. 3.2, is very similar for all loops. This is illustrated in Fig. 6, which displays the temperature profiles of three different loops corresponding to the respective minimal mean temperatures.



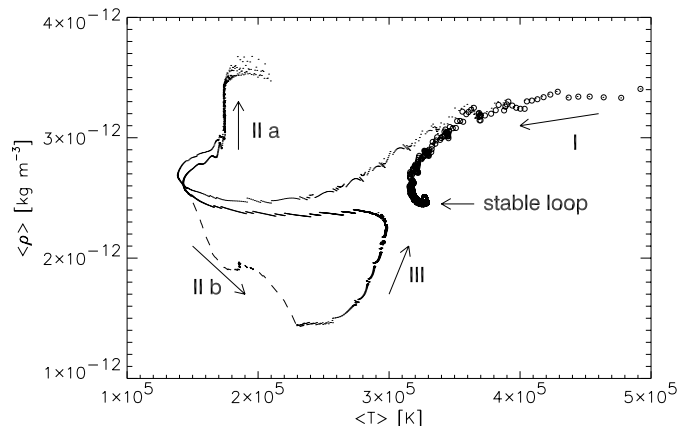
**Fig. 6.** Temperature profiles of different loops at the time when a condensation region has formed. *Solid line:*  $H_m = 1.25$  Mm, *dotted line:*  $H_m = 1.0$  Mm, *dash-dotted line:*  $H_m = 0.75$  Mm.

As shown in Fig. 5, the period of the condensation cycle depends on the damping length – the more the heating is localized near the footpoints, the sooner the thermal instability sets in.

### 3.5. Limit cycle of loop evolution

As pointed out previously, the thermal evolution of the model coronal loop shows periodicity for a significant parameter range of the damping length. To illustrate this cyclic pattern, we plot in Fig. 7 the mean density,  $\langle \rho \rangle$ , of the loop as a function of mean loop temperature,  $\langle T \rangle$ . From here on, we define the mean values as the average quantities over the region of the loop which lies above the transition region, bounded by the points where the temperature crosses  $T = 10^5$  K in both loop legs. The exact choice of this cut-off value does not significantly influence the results and could be set to any temperature  $T > 2 \times 10^4$  K. In contrast to the convention used in the previous section, this definition is independent of motions of the chromosphere–transition region boundary, while the former definition was used to describe the decaying loop together with the other solutions. Figure 7 displays the loop evolution for two different damping lengths: for  $H_m = 1.50$  Mm, the loop approaches a stationary solution (*open circles*), while for  $H_m = 1.25$  Mm (*dots*), the loop enters a limit cycle after its initial cooling, expressing the fact that the loop evolution becomes independent of the initial boundary conditions. The evolution can be divided into four parts:

- I The 10 Mm loop first cools down from its initial mean temperature of  $\langle T \rangle_0 = 5 \times 10^5$  K to  $\langle T \rangle \approx 1.4 \times 10^5$  K.
- IIa The onset of condensation is seen as an increase in the mean density of the loop. The mean temperature starts to rise again shortly before the condensation region leaves the loop, which is due to the fact that one side of the loop is already reheating while the condensation region is moving to the other side. The stage of evolution when the condensation region drains from the loop is seen as a sudden drop in density from  $\langle \rho \rangle = 3.6 \times 10^{-12}$  kg m $^{-3}$  to  $\langle \rho \rangle = 1.4 \times 10^{-12}$  kg m $^{-3}$ . One point is plotted for each 10 s of the



**Fig. 7.** Limit cycle of loop evolution for a damping length of  $H_m = 1.25$  Mm (*dots*) and  $H_m = 1.50$  Mm (*open circles*). The phases of evolution are indicated as follows: (I): initial cooling, (II a) condensation, (II b) simultaneous evolution of the hot part of the loop (*dashed line*), (III) loop reheating and chromospheric evaporation.

evolution, and the lack of points in this fairly large interval of mean density illustrates that the condensation region leaves the loop very quickly (but still with a velocity that is much slower the free-fall velocity of  $v_{ff} = 31.2$  km s $^{-1}$  for this loop).

- IIb As the mean density of the loop during the condensation phase is dominated by the condensation region itself, we also evaluated the density in the hot part of the loop alone: due to the formation of a condensation region, the density in the adjacent parts of the coronal loop decreases which leads to an increase in temperature. The mean values of the hot part of the loop for this stage of evolution is plotted as a *dashed line* in Fig. 7.
- III After the condensation region has drained, the evacuated loop reheats and chromospheric matter is evaporated, as indicated by the increase in mean density. When the loop reaches  $\langle T \rangle = 3 \times 10^5$  K, the radiative losses at the loop top are no longer balanced by the energy supply through mechanical heating, conductive flux, and enthalpy flux, so that the temperature starts to decrease and the cycle repeats.

Cyclic evolution of coronal loops was studied for the first time by Kuin & Martens (1982). In their semi-analytical model, they treated the coronal loop as a zero dimensional system, coupled to the underlying chromosphere. Depending on the strength of the coupling, the authors obtained different classes of solutions, namely solutions converging towards a fixed point, and solutions approaching a limit cycle. As the loop was treated as one zero dimensional system, however, Kuin & Martens were not able to model any spatially localized condensation which in our work leads to the upward-arching branch in the  $\langle \rho \rangle$ – $\langle T \rangle$  diagram of Fig. 7. Considering the hot coronal part of the loop alone, in contrast, reconciles our spatially resolved loop model with the semi-analytical approach of Kuin & Martens (cf. Fig. 7, *dashed line*).

### 3.6. Remarks on Rayleigh-Taylor instability

Loop configurations with a density inversion at the center are unstable against Rayleigh-Taylor instability if  $\nabla\rho \cdot \mathbf{g} < 0$ . The question is: would a Rayleigh-Taylor instability inhibit the condensation of plasma in the upper part of a coronal loop? To estimate the importance of Rayleigh-Taylor instability compared to the dynamic time scale of our model loop, we follow the work of Chandrasekhar (1961) and calculate the growth rate,  $\omega$ , of the amplitude of normal modes of the form  $A(\mathbf{x}, t) \propto \exp[i(k_x x + k_y y) + \omega t]$  as a result of a density perturbation near the boundary between two incompressible, inviscid fluids of uniform densities,  $\rho_2$  and  $\rho_1$  ( $\rho_2 > \rho_1$ ), permeated by a uniform magnetic field parallel to the direction of the gravitational force. One finds that an upper limit for the growth rate,  $\omega$ , of the perturbation is given by

$$\omega_{\max} = \frac{\sqrt{4\pi\mu g_{\parallel}}}{B_0} (\sqrt{\rho_2} - \sqrt{\rho_1}). \quad (7)$$

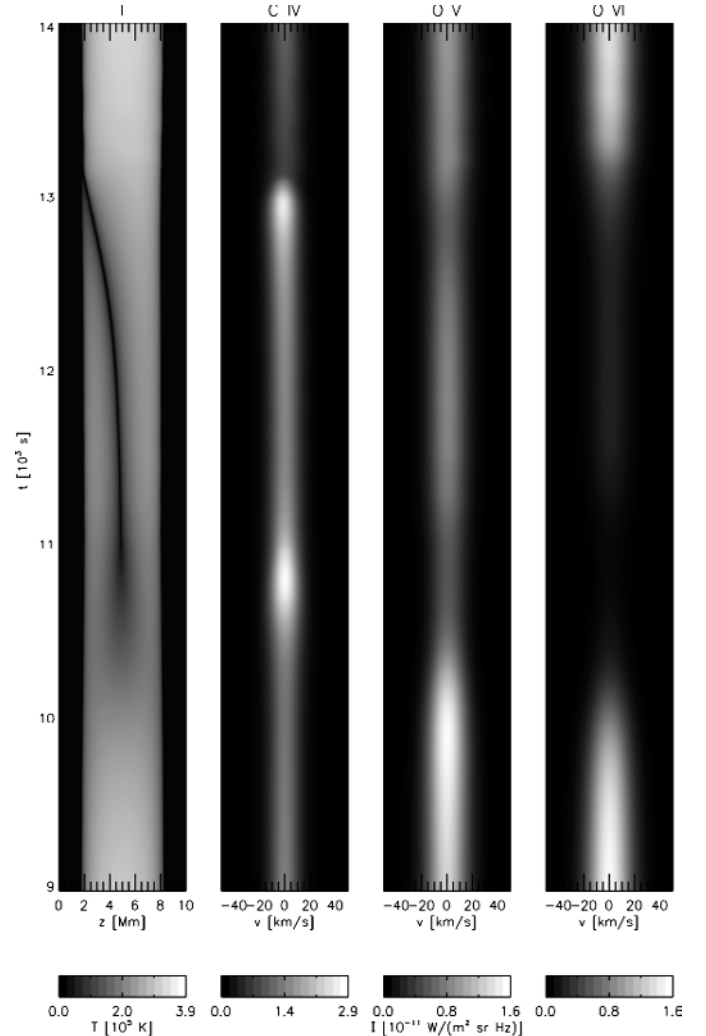
Inserting typical values for the formation of a condensation region of  $\rho_1 = 3 \times 10^{-12} \text{ kg m}^{-3}$ ,  $\rho_2 = 4 \times 10^{-11} \text{ kg m}^{-3}$ ,  $g_{\parallel} = 0.04 \cdot g_{\odot}$  (corresponding to a width of the condensation region of 0.2 Mm), and  $B_0 = 10 \text{ G}$ , we obtain a time scale of  $T = \frac{2\pi}{\omega} \approx 22\,000 \text{ s}$ , which is more than an order of magnitude larger than the time scale over which the condensation region evolves. We thus conclude that the onset of Rayleigh-Taylor instability does not fundamentally affect the formation of the condensation region. It might eventually lead to a dissolution of the condensation region, but at that stage, this region is already moving towards the loop footpoint, which would also happen if the condensation were split up in pieces.

Moreover, we have checked that the perturbation of the loop geometry due to the accumulation of mass in the center of the loop is negligible.

### 3.7. Spectral signature of condensation in transition region lines

The fact that our numerical code self-consistently solves the non-equilibrium ionization rate equations not only for hydrogen and helium, but also for the atomic species C, O (and Fe, Mg, N, Ne, and Si, if desired) offers the possibility of synthesizing optically thin transition region lines. The inclusion of non-equilibrium ionization effects is of vital importance when studying the spectral signature of a plasma in a *dynamic* state like in the present case.

Figure 8 displays the intensity variations of the lines CIV 1548 Å (formed at  $T \approx 1 \times 10^5 \text{ K}$ ), OV 630 Å ( $T \approx 2.2 \times 10^5 \text{ K}$ ), and OVI 1032 Å ( $T \approx 3.2 \times 10^5 \text{ K}$ ) during the evolution of the loop. The spectral lines are calculated by integrating the emission of the entire loop as seen vertically from the top, the line widths are given in velocity units. All three lines show periodic brightenings which have their origin in the condensation process. In the case of the CIV line, the strong increase in density at the beginning of the condensation results in high radiative losses and hence an intensity maximum. A second maximum of slightly smaller amplitude is attained when the condensation region has grown to its



**Fig. 8.** From left to right: space-time plot of the loop temperature and the corresponding variations of the lines of CIV 1548 Å, OV 630 Å, OVI 1032 Å for a damping length of  $H_m = 1.25 \text{ Mm}$ .

maximum, shortly before draining down the loop leg. Right after the condensation region has left the loop, the intensity is minimal as the loop is devoid of plasma at this stage. In the following evolution, the intensity gradually increases as chromospheric evaporation sets in again. In contrast to this, the intensity of the OVI line is maximal when the temperature is highest as the line is formed around  $T \approx 3.2 \times 10^5 \text{ K}$ . When the condensation sets in and the maximal loop temperature temporarily sinks below  $T = 2 \times 10^5 \text{ K}$ , the intensity in OVI almost drops to zero. The OV line, formed around  $T \approx 2.2 \times 10^5 \text{ K}$ , can be considered as an intermediate case.

For a damping length of  $H_m = 1.25 \text{ Mm}$ , the CIV total intensity varies between  $1.1 \text{ W}/(\text{m}^2 \text{ sr})$  and  $3.8 \text{ W}/(\text{m}^2 \text{ sr})$ , the OV total intensity varies between  $2.0 \text{ W}/(\text{m}^2 \text{ sr})$  and  $6.9 \text{ W}/(\text{m}^2 \text{ sr})$ , while the OVI total intensity varies between  $0.1 \text{ W}/(\text{m}^2 \text{ sr})$  and  $4.8 \text{ W}/(\text{m}^2 \text{ sr})$ . The observed Doppler shifts are small as the chosen viewing angle is largely perpendicular to the direction of motion in the loop and the velocities are small. For shorter damping lengths, the maximum temperatures of the loop are lower which results in a *decreased*



intensity for lines which are formed at higher temperatures. The O VI line, e.g., shows bright periodic intensity maxima for  $H_m = 1.25$  Mm, while it is almost invisible for a damping length of  $H_m = 0.75$  Mm. In contrast to this, the intensity range of the C IV line remains almost unaffected by a change of the damping length as the maximum loop temperature exceeds in all cases its formation temperature.

#### 4. Discussion

We have shown that cool coronal loops can exhibit inherently dynamic behavior even under the simple assumption of a mechanical energy flux into the loop that is dissipated exponentially with a given scale height but constant in time. This scenario is interesting in the sense that no time-dependent driving mechanism is needed to generate transient brightenings in transition region lines. Simultaneous observations of, e.g., the C IV 1548 Å and the O VI 1032 Å lines, would be advantageous in order to verify if this phenomenon is as ubiquitous as it seems.

Recent TRACE observations of Schrijver (2001) indeed show frequent “catastrophic cooling” and evacuation of coronal loops over active regions and enhanced emission of C IV, developing initially near the loop top, followed by quick draining. Furthermore, CDS observations by Fredvik (2002) show localized brightenings in coronal loops in OV 630 Å on the limb which move quickly towards the solar surface and could be interpreted as cooling plasma close to a condensation region. As most of these recent observations refer to loops that are about one order of magnitude larger than those considered here, further work is on its way to study the dependence of the condensation process on the loop length. This could also help to better understand and disentangle loops of different lengths in active regions, as observed, e.g., by Spadaro et al. (2000).

The fact that the dynamic loop models described in this work can show strong emission in lines formed at  $T \leq 10^5$  K and at the same time relatively weak emission in lines formed at higher temperatures seems promising with respect to the outstanding problem that current models predict an emission measure that is either much lower than the emission observed at  $T < 10^5$  K or much higher than what is observed at  $T > 10^5$  K.

Further observational confirmation of the dynamics predicted in this paper, preferably concentrating on shorter loops, would lead to a strengthening of the hypothesis that coronal heating is concentrated towards the footpoints of loops. Such knowledge would be very useful to limit the number of possible coronal heating mechanisms.

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